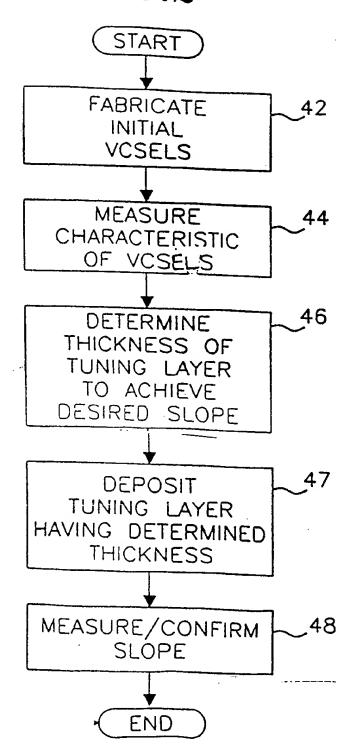
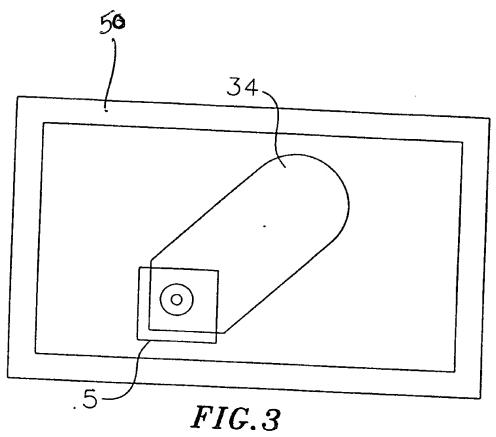


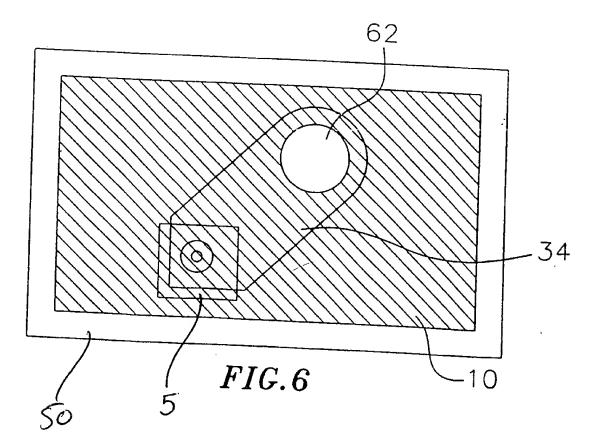


FIG.2

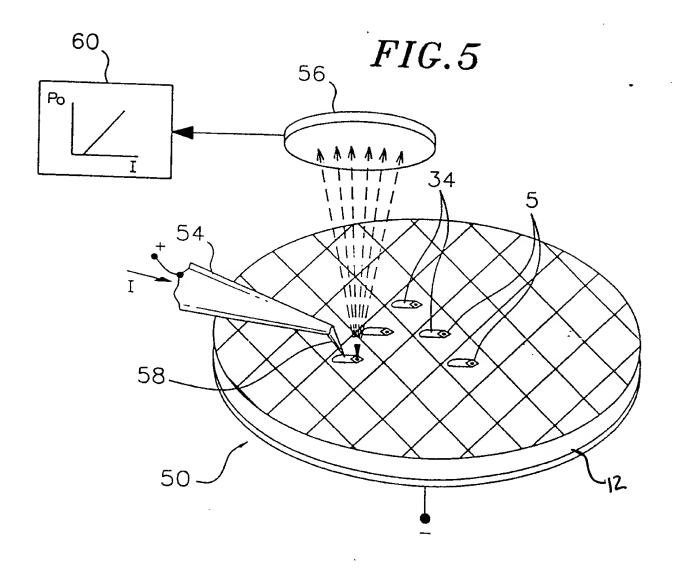












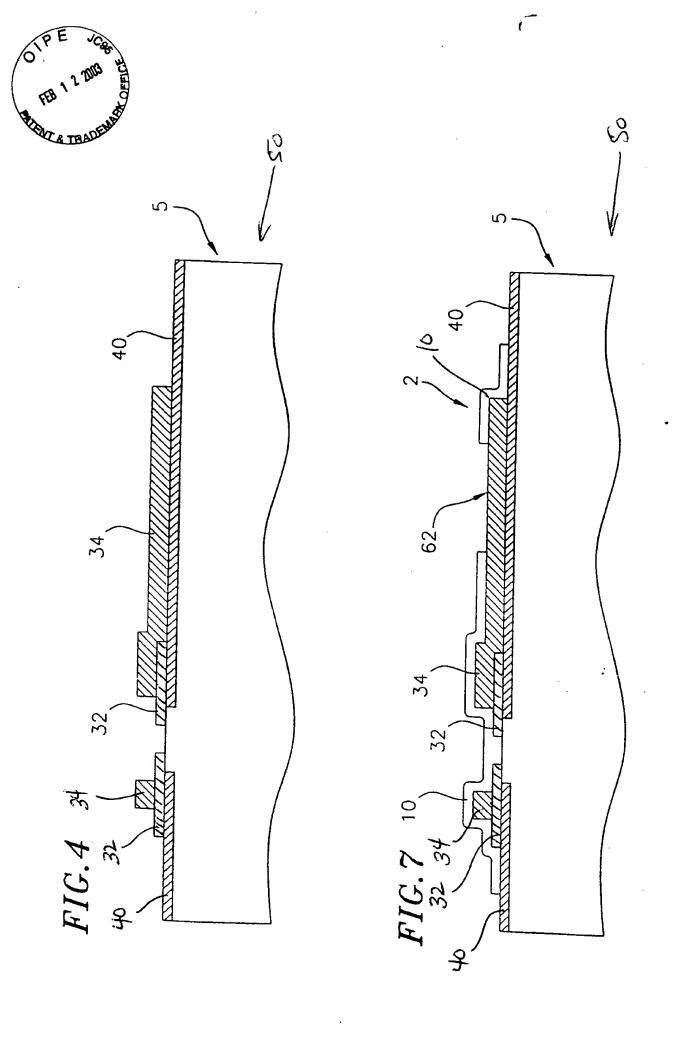




FIG.8

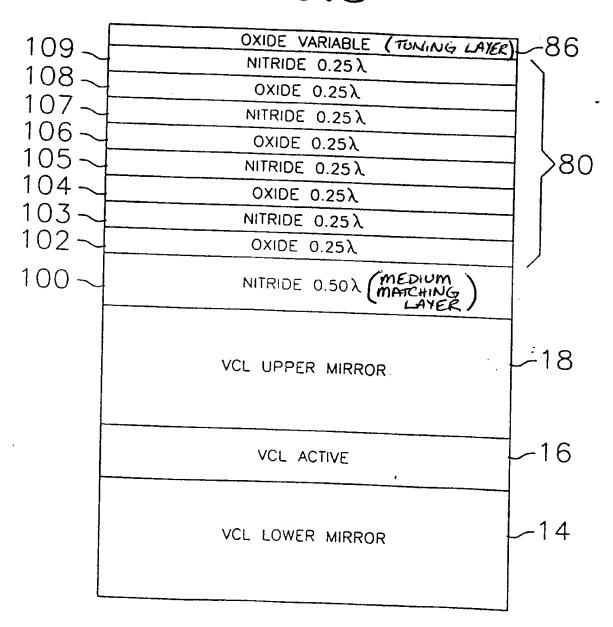
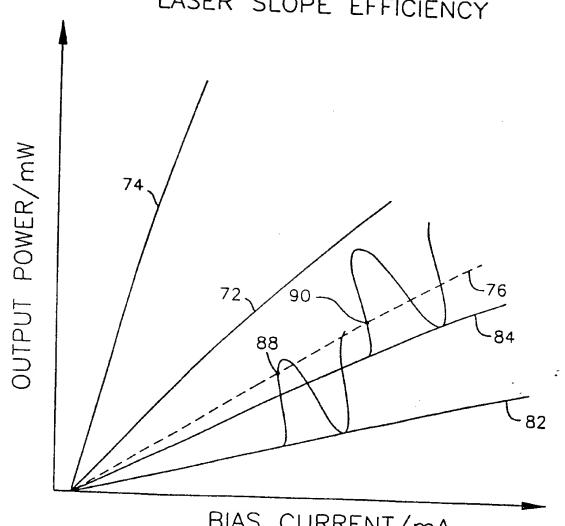


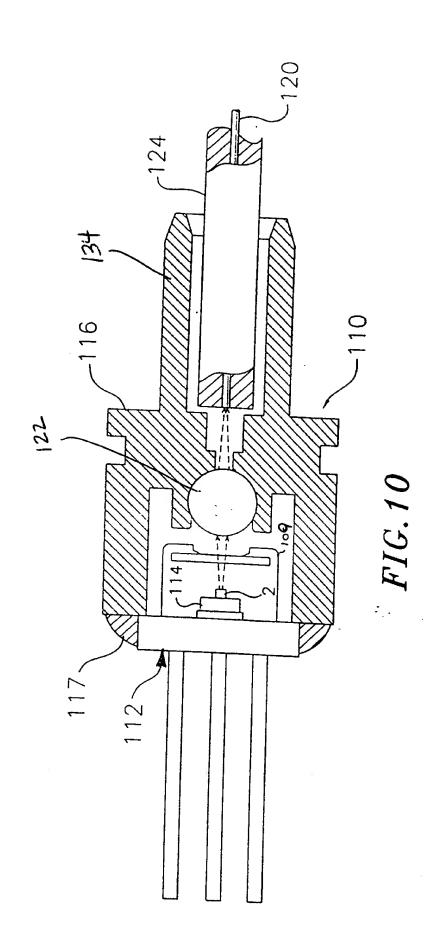


FIG.9LASER SLOPE EFFICIENCY



BIAS CURRENT/mA





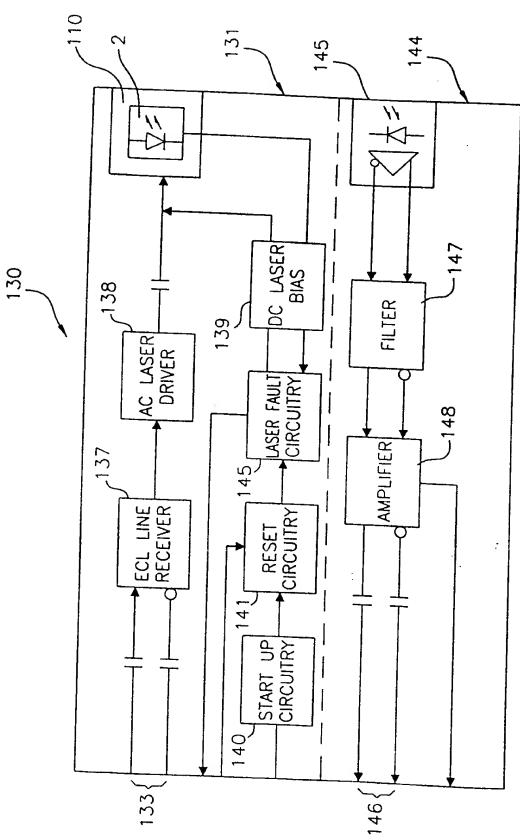
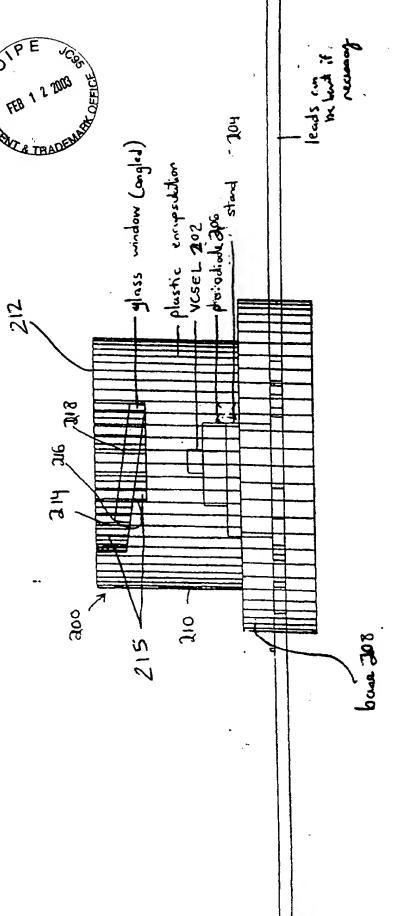


FIG. 11

VCSEL PACKAGE PLASTIC ENCAPSULATION WANGLED WINDOW

Plastic encapsulation replacement for TOSG purchage without impacting other poducying cufit



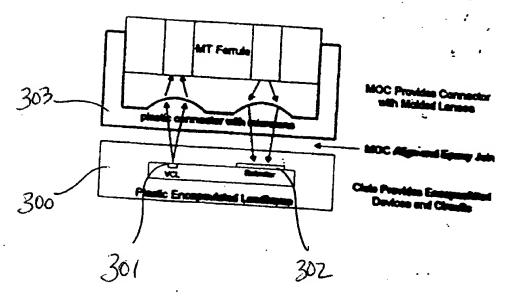
FI6.12



FIG. 13

Small Form Factor Concept

FLASTIC ENCAPSULATED





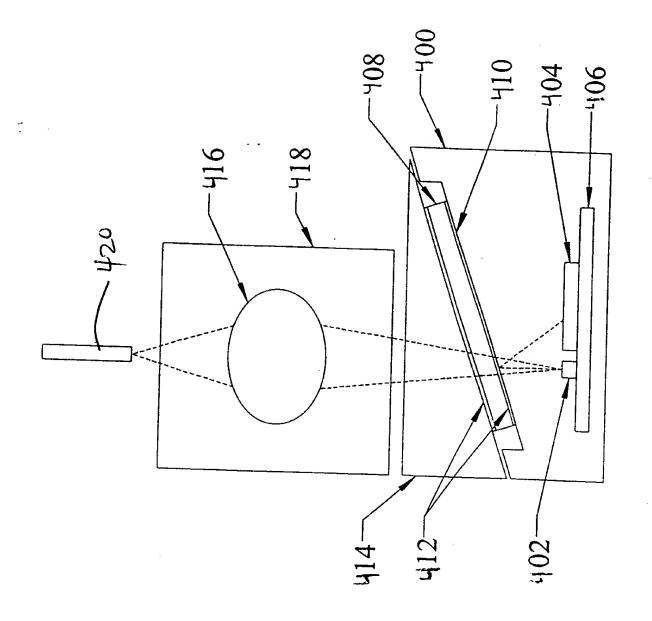
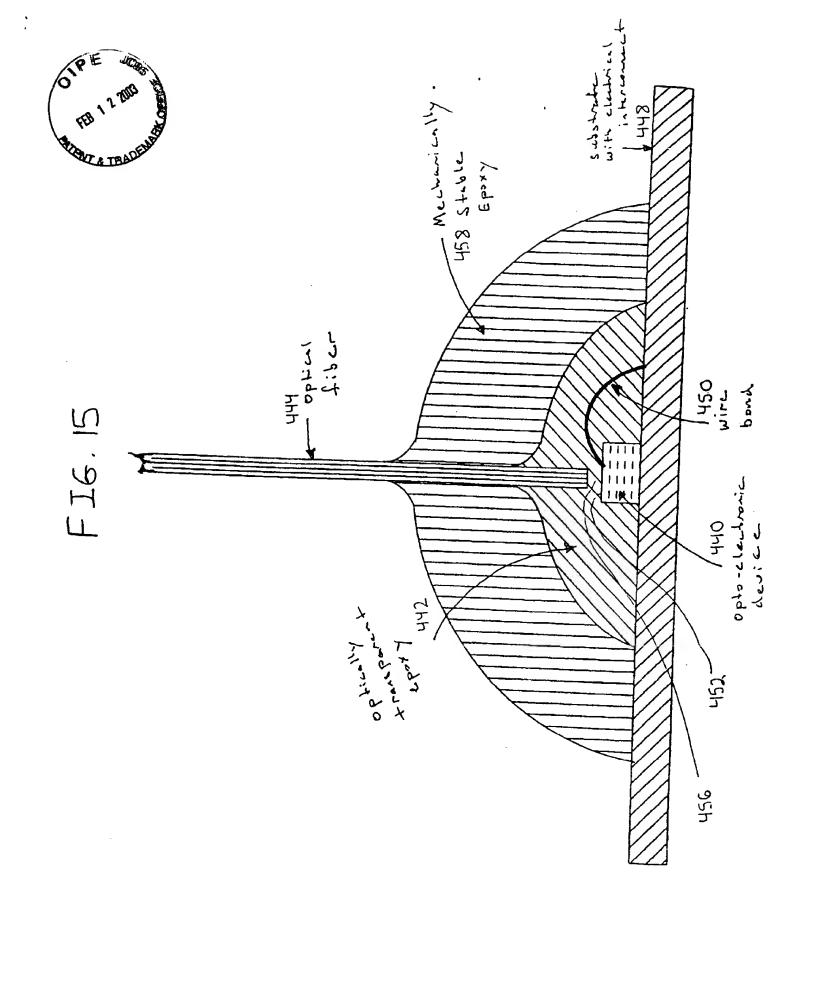
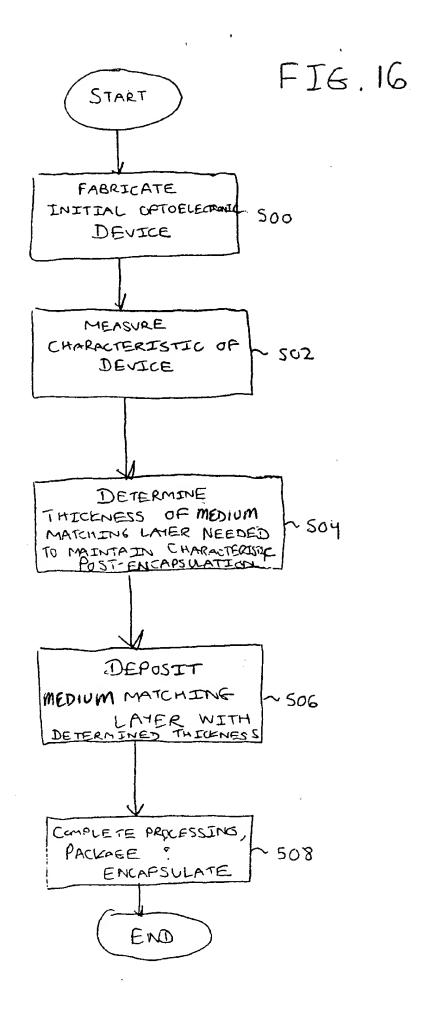


FIG. 14



21076 1174

OIP : CONTRACTOR





VCSEL structure	Oxide Medium Match Thickness (A)	Transmission in air (%)	Transmission in plastic (%)
4 periods +	0	0.017	0.025
4 periods +	200	0.017	0.025
4 periods +	400	0.018	0.025
4 periods +	600	0.020	0.024
4 periods +	800	0.023	0.024
4 periods +	840	0.024	0.024
4 periods +	1000	0.027	0.024
4 periods +	1200	0.032	0.023
4 periods +	1400	0.034	0.023

FIG. 17

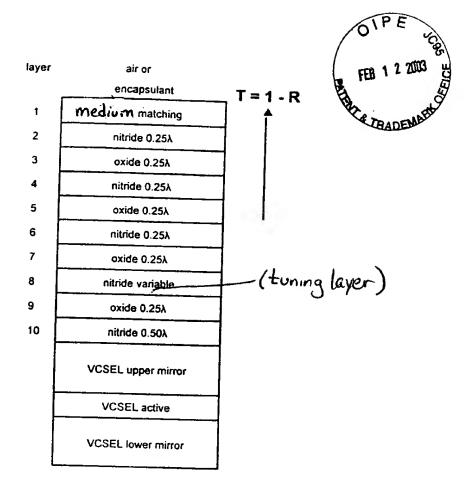


FIG. 18

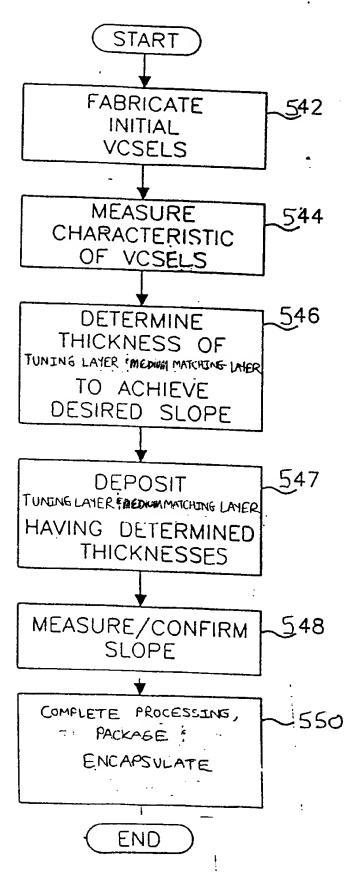
Funing Layer Thickness (layer 8)	Medium Match Thickness (layer 1)	Transmission in air or plastic	Loss	Optical Efficiency	Scaled
as grown	No mirror	0.256	0.3	0.460	1
1062	840	0.024	0.3	0.074	0.161
850	1050	0.025	0.3	0.077	0.167
637	1300	0.029	0.3	0.088	0.191
425	1550	0.036	0.3	0.107	0.233
212	1930	0.042	0.3	0.123	0.267
0	2330	0.045	0.3	0.130	0.283



FIG. 19

FEB 1 2 7000 AND THE PER 1 7000 AND THE PER 1 2 700

FIG. 20





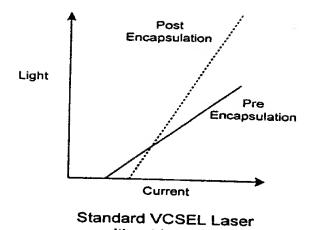


FIG. 21

without invention

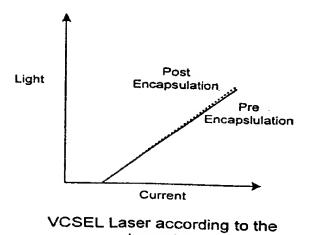


FIG. 21A

invention

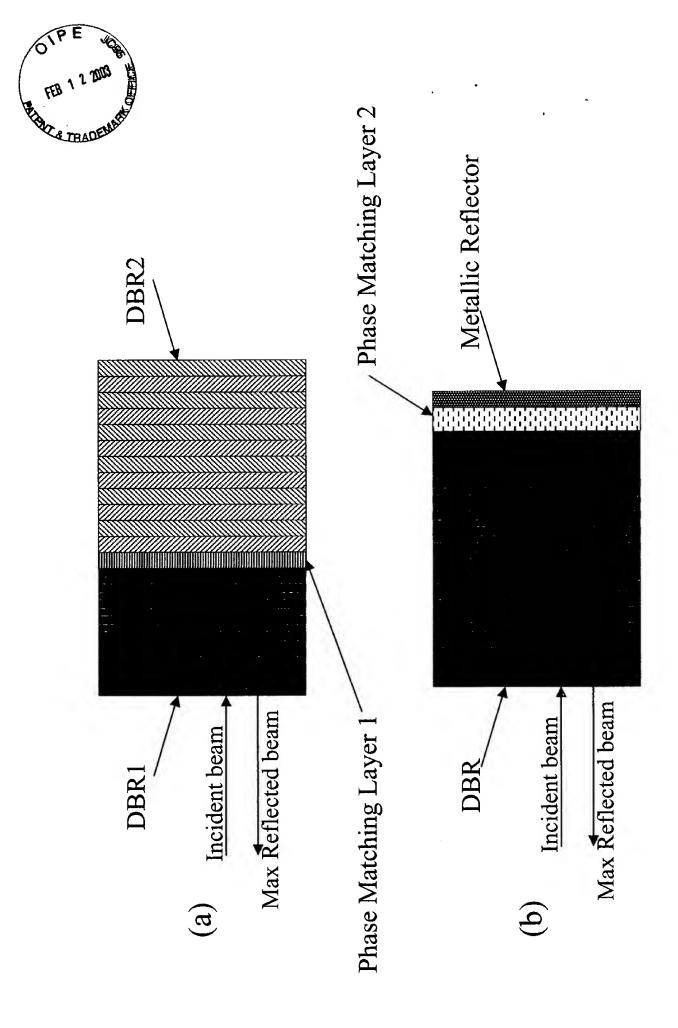


Figure 1. Prior Art Phase-Matching Layers



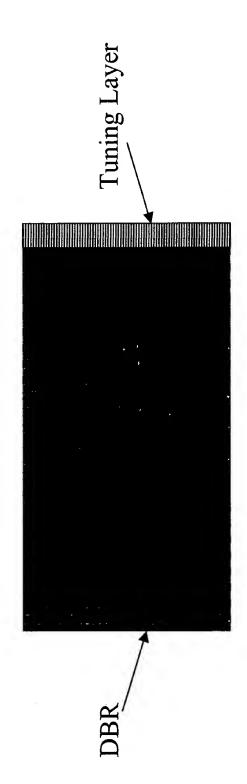


Figure 2. Prior Art Tuning Layer



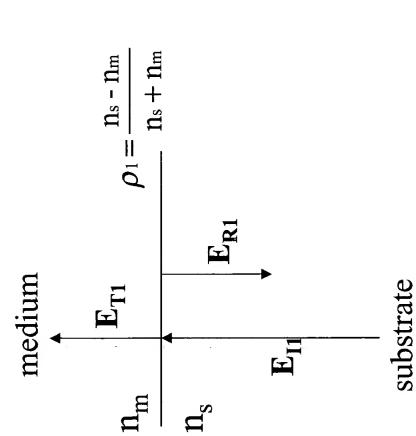
$$R_2 = (\rho_2)^2$$

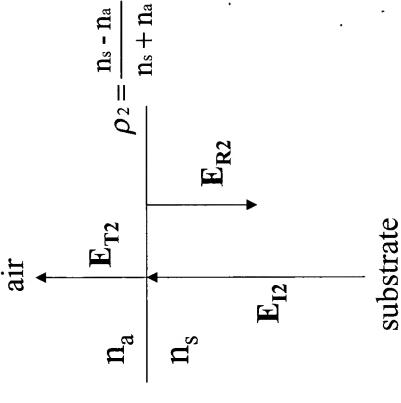
 $R_2 = 1 - R_2$



 $T_1 = 1 - R_1$

 $R_1 = (\rho_1)^2$





NOTE: $R_1 \neq R_2 \& T_1 \neq T_2$, because $n_m \neq n_a$

Figure 3. Elementary Example of the Problem

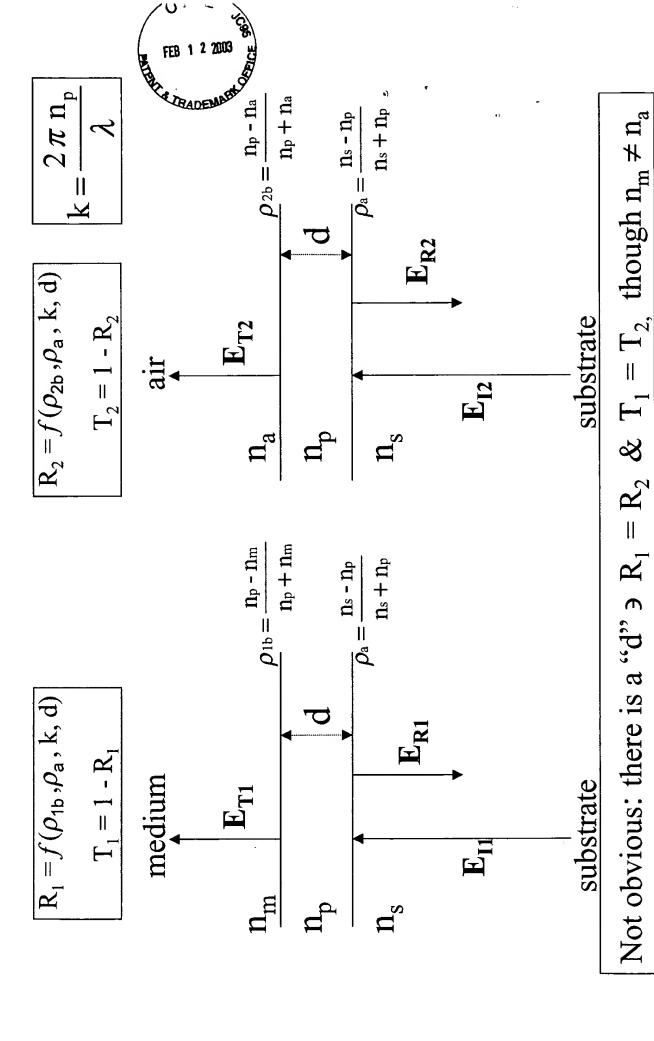


Figure 4. Elementary Example of the Solution

$$R_1 = \frac{(\rho_a + \rho_{1b})^2 - 4\rho_a \rho_{1b} \sin^2 kd}{(1 + \rho_a \rho_{1b})^2 - 4\rho_a \rho_{1b} \sin^2 kd}$$

$$R_2 = \frac{(\rho_a + \rho_{2b})^2 - 4\rho_a \rho_{2b} \sin^2 kd}{(1 + \rho_a \rho_{2b})^2 - 4\rho_a \rho_{2b} \sin^2 kd}$$

Figure 5. Formulas for the R1 & R2 in figure 4